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## (54) Powder coating cellulose fibre substrates

(57) A cellulose fibre substrate such as a wood based material is coated by depositing a coating powder on it to form a coating and then using radiant heat to cure the coating powder. The coating powder typically contains a resin with a curing agent and, preferably, an adjuvant, such as a plasticiser or a wax, for lowering its softening temperature. The coating powder is preferably applied by an electrostatic method and the radiant heat is preferably applied in the form of infra-red radiation, typically having a wavelength in the region of from 1 to 5 microns.

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## **SPECIFICATION**

## Coating cellulose fibre substrates

5 This invention relates to the coating of substrates made from cellulose fibre materials such as, 5 for example, timber articles wooden boards, chipboard, hardboard, cardboard and paper. The high cost of solvents for conventional liquid coatings has made the use of powder coatings more attractive. However, although powder coatings have been used for some time for coating metal articles using electrostatically charged powder the attraction to the metal depends 10 on its electrical conductivity and it has been thought impossible to use the same techniques for 10 wood based substrates because they are substantially non-conducting. Another difficulty with the application of powder coatings on wood is that of applying heat to melt and cure the powder. For metal articles, this heat is usually supplied by gas, oil or electrically heated convection ovens, but this heat can affect a wood based substrate by causing moisture, sap or 15 resin to be exuded causing defects in the coating. Also changes in the physical dimensions of 15 the substrate can occur due to drying. It is an object of the present invention to provide a process for using powder coating for coating a cellulose fibre substrate. According to the present invention there is provided a method of coating a cellulose fibre 20 substrate including the steps of depositing a resin-containing coating powder onto the substrates 20 to form a coating thereon and subsequently using radiant heat to cure the coating on the substrate. In one especially preferred embodiment of the present invention, the coating powder is applied by an electrostatic charge process. In this respect, although the cellulose fibre substrates 25 have low electrical conductivity, it has been found that their conductivity is sufficient for a 25 coating powder as defined above to adhere to the surface, provided that either the substrate is of sufficient thickness to have adequate electrical conductivity for a single earthing point to be sufficient or the substrate is backed by an earthed conductive support, (which may be a sheet or non-continuous, such as a cross-rod conveyor) or has a plurality of earthing points distributed 30 over it. 30 The powder is advantageously applied by an electro static spray technique but other methods, such as fluidised bed techniques, may also be employed. A coating of powder can also be produced by allowing the powder to fall on to the substrate without using electrostatic attraction, for example by using a vibratory hopper. This is 35 particularly suitable for coating one surface of a substantially flat sheet, so that the powder is 35 held on the substrate by gravity. Alternatively, the powder may be applied by other methods such as fluidised bed techniques. The radiant heat may be applied by ultra-violet irradiation or electron beam irradiation but is preferably applied by infra-red irradiation from suitable lamps and it has been found that 40 wavelengths in the region from 1.0 to 5 microns provide the best curing of the powder coating 40 without overheating the substrate. Wavelengths in the range of from 1.0 to 1.5 microns are generally preferred but infra-red radiation having a wavelength in the region 1.5 to 5 microns can be used and produces good results. Intensities of the shorter wavelength infra-red radiation found suitable are about 2 to 10 watts per centimetre of lamp length and 1 to 5 watts per 45 centimetre of lamp length for the longer wavelength radiation. A suitable distance of the lamps 45 from the substrate is from 2 to 20 cm, a shorter distance than this having been found to cause scorching of the powder and a greater distance having been found to cause the substrate to overheat before the powder is fully cured. The term "cellulose fibre substrate" includes, for example, wood, timber, chipboard, particle 50 board, fibre board, hardboard, cardboard, plywood, veneer, block board (which board products 50 may be paper-faced) and paper, including articles made from regenerated cellulose. Such substrates may, as in certain commercially available materials, especially chipboard and particle board, be pretreated, eg by impregnation or coating with a resin such as a polyester, polyurethane or alkyd resin. However, in accordance with the present invention, the coating 55 powder is applied directly onto the substrate. That is to say, it is not necessary to apply a 55 protective layer of resinous, eg polyester resin, material to such compressed boards before the coating powder is applied. The invention is especially suitable for coating a substrate of any wood based material. Such material has a small electrical conductivity due to its water content which, it is believed, enables the substrate to provide, if required, adequate electrostatic 60 attraction for the powder. If the substrate is relatively thick then the electrical capacitance of the 60 substrate has been found to be adequate to hold the electrostatically charged coating powder whilst it is cured by radiant heat, using a single earthing point on the substrate. If, however, the substrate is thin then it is preferable to provide an electrically conductive backing which is

connected to earth or at least a plurality of distributed earth points so that the electrostatic

65 charge induced into the substrate by the coating powder can be discharged to earth.

	The powder may be applied by an electrostatic spray gun to the substrate using conventional	
	powder spraying equipment such as that known by the names Volstatic, Gema and Controsion.  Alternatively the powder may be placed in a vibratory hopper under which the substrate to be	
	coated is passed, the hopper being maintained at a suitable electrical potential to provide the	
5	required electrostatic charge to the particles sufficient to give a thin even film of powder on the	5
	surface of the substrate, or by a pure electrostatic method, eg by using the Brennenstühl	
	apparatus. Alternatively the powder may be placed in a vibratory hopper under which the substrate to be coated is passed, using gravity rather than electrostatic charging to apply an	
	even film of powder. The substrate whilst being coated with powder using an electrically	
10	charged spray may be hung vertically from a fixed point or a conveyor to provide an earthing	10
	point for the substrate. Several earthing points would be provided for large areas or thinner	
	sheets so as to provide adequate electrical conductivity from the surface being coated to earth.  Alternatively the substrates may be coated in a horizontal position using a flat conveyor passing	
	the sheets under fixed or reciprocating electrostatic spray guns. The conveyor may have an	
15	electrically conductive support for the substrate so as to provide a good earth connection over	15
	the back face of the material.	
	After the powder coating is formed on the substrate it is cured by subjecting the powder film to radiant heat, preferably in the form of infra-red radiation. It has been found that the	
	wavelength, intensity and separation of the lamps from the substrate need to be selected	
20	carefully to ensure a good flow of the coating during curing and to complete the cure of the	20
	coating without overheating the substrate. Infra-red lamps producing radiation in the wavelength	
	range from 1.00 to 1.5 microns may be provided spaced from 2 to 20 cms from the substrate so as to provide a power intensity of from 2 to 10 watts per centimetre of lamp length and	
	preferably about 4.3 watts per centimetre. Alternatively the lamps may produce radiation of	
25	wavelength in the range 1.5 to 5 microns and spaced the same distance from the substrate as	25
	for the shorter radiation to produce a power intensity of from 1 to 5 watts per centimetre of	
	lamp length and preferably about 2 watts per centimetre.  It has been found that using the coating compositions described below a period of between	
	45 seconds and 2 minutes is required for a white powder coating and from 20 seconds to 2	
30	minutes, especially 30 seconds to 1½ minutes, for a black powder coating to effect curing of the	30
	coating.	
	Although, in principle, it has been found that many commercially available powder coating materials can be applied electrostatically to cellulose fibre substrates with varying degrees of	
	success and can be caused to flow and cure by using applied radiation as described above it has	
35	been found that greatly superior coatings can be obtained using coating compositions which are	35
	specifically intended for the purpose.  Thus the preferred coating compositions used in the present invention comprise a thermosett-	
	ing resin, together with suitable curing agent, and an adjuvant which reduces the softening	
	temperature of the resin composition, for example a flow agent, a plasticizer, or, preferably a	
40	wax, or a combination of two or more such materials. Formulating the coating composition with	40
	the above-mentioned ingredients, it is possible, especially when electrostatic application and infra-red radiation curing methods are employed, to obtain surface coatings which exhibit a	
	greatly enhanced appearance and surface hardness, as measured, for example, by using the	
	FIRA BS 3962 scratch test. This degree of surface hardness gives an excellent resistance to	
45	scuffing, coin marking and handling, but still provides the adhesion and flexibility necessary for sawing and drilling operations.	45
	The thermo setting resin is preferably a polyester resin, but other resins may be employed.	
	The resin used should preferably have a softening temperature between 70°C and 120°C, a	
<b>E</b> 0	Tg of between 40°C and 80°C, a melt index between 2 gm/min and 30 gm/min (ASTI	50
50	D1238–62T) and a density of 1.1 to 1.4 gm/ml at 23°C. If the resin is a polyester it may incorporate esters of terephthalic and similar polyacids and polyols such as glycols with from 2	50
	to 10 carbon atoms. The curing agents may be mainly functional through glycidyl groups, i.e.	
	so as to produce a pure polyester, and may be trifunctional materials such as Triglycidyl	
	Isocyanurate (TGIC) and Tri(epoxy propyl) Isocyanurate (TEPIC). Other suitable curing agents	55
DD	include epoxy resins of epoxide equivalent between 400 and 1,000, and isocyanates, which produce polyurethanes.	99
	Alternative coating powders may be based on other resins, e.g. epoxy resins, such as those	
	cured with substituted or unsubstituted dicyandiamides, amines, amidines or anhydrides;	
60	acrylics; epoxy-phenolics; epoxy-novolacs and epoxy-resols; the curing systems may in some cases contain an accelerator.	60
50	In general the coating powder will incorporate a flow agent to reduce its surface viscosity. The	50
	flow agent is typically employed in a proportion known to those in the art, for example, in an	
	amount of at least 0.1 parts by weight based on 100 parts of the resin, and advantageously in	•
65	an amount of from 0.2 to 10 parts, especially from 0.4 to 5 parts, although the exact amount employed will, of course, depend on the nature of the resin, the flow agent, and the other	65
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5	ingredients of the coating powder. Amongst suitable flow agents there may be mentioned, for example, polyacrylates, fluorocarbon polymers, silicone polymers, polyvinyl butyral polymers etc. The preferred coating powders incorporate a plasticiser or, more especially, a wax, to bring about a reduction in softening temperature.  The wax component is advantageously present in an amount of up to 10 parts and preferably of at least 0.1 parts by weight per 100 parts of resin, amounts in the range of from 0.5 to 10 parts, especially from 1 to 5 parts, being preferred, although, again, the optimum amount used	5	
10	will depend on the nature of the wax and the other components of the coating powder. Amongst suitable natural or synthetic waxes there may be mentioned, for example, polyolefin waxes, e.g. polyethylene and polypropylene waxes, amide waxes, e.g. bis-stearamide, gums and other high molecular weight materials, including crystalline and microcrystalline waxes.  Depending on the application concerned, the coating powders may also comprise various other ingredients, including, especially, pigments for coloured coatings and non-pigmenting	10	
15	fillers as extenders. Amongst suitable pigmenting fillers there may be mentioned, titanium dioxide, carbon black, iron oxides, lithopone, zinc oxide and pigments based on cadmium, lead or chromium, as well as organic pigments such as phthalocyanines, azo and dioxazine dyestuffs etc.; amongst suitable extenders there may be mentioned, for example, calcium carbonate and	15	
20	The pigments are preferably employed in amounts of from 0.5 to 100 parts by weight per 100 parts of resin, typically from 10 to 50 parts. It should be emphasized, however, that the present invention also provides clear finishes, in which case the pigment may be excluded. The extenders, if present, are typically employed in amounts of up to 100 parts by weight per 100	20	
25	parts of resin, especially from 5 to 50 parts, although amounts of up to 200 parts by weight may be used for so-called "flat" finishes.  Lower proportions of the fillers and the extenders will normally be employed when the method of the present invention is used to coat paper products.  In addition, the coating powders may include other ingredients which may be added, for any	25	
30	given purpose, including, for example, plasticizers, ultra violet absorbents, accelators, anti- cratering agents, catalysts and fungicides etc.  A typical white coating powder for use in the present invention comprises; 100 parts by weight resin, e.g. polyester 4–20 parts by weight curing agent, e.g. triglycidyl isocyanurate	30	
35	0.2–2 parts by weight flow agent, e.g. triglycidyl isocyanurate 0.2–2 parts by weight flow agent, e.g. polyacrylate 10–80 parts by weight pigment, e.g. titanium dioxide 0–60 parts by weight extender, e.g. calcium carbonate 0.1–10 parts by weight wax, e.g. polyethylene. A typical black coating powder for use in the present invention comprises;	35	
40	100 parts by weight resin, e.g. epoxy, 2-10 parts by weight curing agent, e.g. amine 0.2-2 parts by weight flow agent, e.g. polyacrylate 0.1-0.6 parts by weight pigment, e.g. carbon black 0-60 parts by weight extender, e.g. calcium carbonate	40	
45	0.1–10 parts by weight wax, e.g. polyethylene.  The coating powders may be formulated by conventional techniques, for example, by premixing the components in a blender, extruding the blend and then grinding the extrudate; the preferred particle size being in the range of from 1 to 75 microns.  The following Examples illustrate the invention, parts being by weight.	45	
50	Example 1  The following samples illustrate coating powders which are suitable for use in the present invention.	50	

	A White Coatin	na Powder				
				Parts		
			Typical	Preferred Ranges		
5	Resin	Polyester	100	100		5
	Flow agent	Polyacrylate	1	0.4-1.6	,	
	Curing agent	TGIC	7	5-15		
	Pigment	Titanium Dioxide	48	20-80	•	
	Filler	Calcium Carbonate	43	0-60		
10	Wax	Polyethylene	3	1–6		10
	B Black Coatin	a Powder				
	Resin	Polyester	100	100	•	
	Flow agent	Polyacrylate	1.2	0.6-1.8		
15	Curing agent	TEPIC	7.1	4-15		15
. •	Pigment	Carbon Black	2.1	0.75-6		
	Filler	Barium sulphate	37.5	0-60	•	
	Wax	Polypropylene	3.1	0.75-4.5		
20			100	100		20
	Resin	Polyester	100	100		
	Curing agent	Blocked isocyanate	17.6	12-22		
	Flow agent	Flurocarbon	1.7	0.75-3.5		
0.5	Accelerator	Amidine	0.36	0-2.5		0.5
25	Wax	Amide	2.3	0.1-3.6	•	25
	D Beige Textu	red Coating Powder				
	Resin	Ероху	100	100	•	
•	Flow agent	Polyacrylate	0.65	0.4-1.0		
30	Curing agent	Amidine	7	5-10		30
	Filler	Calcium Carbonate	55	40-80		
	Pigments	(Titanium Dioxide	35	20-60		
	-	(				
0.5		(Iron Oxides	4.8	2-20		٥.
35	Wax	Polypropylene	2.3	1–6		35
	E Structured F	inish Coating Powder				
	Resin	Epoxy Novolac	100	100	•	
	Flow agent	Polyacrylate	3.7	1.5-7.5	•	
40	Curing agent	Phenolic	43	35-50		40
	Pigment	Titanium Dioxide	61	50-100		
	Filler	Barytes	35	0-50		
	Wax	Polyethylene	1.5	1.0-4.0		
45	E Pones 0	a Poude-				45
45	•		100	100		45
	Resin	Polyester	100	100		
	Flow agent	Silicone TEPIC	1.15	0.75-2.0		
	Curing agent		7.15	6-15	•	
50	Filler Wax	Calcium Carbonate Amide	3.2	0-60	•	50
50	vvax	Amide	2.9	0.5–6		50
	G Chemical Re	esistant Coating Powder	•			
	Resin	Ероху	100	100		
	Curing agent	Phenolic	33	25-40		
55	Flow agent	Polyvinyl Butyral	4.5	2-10		55
	Pigment	Titanium Dioxide	77	45-90		
	Accelerator	2-Methyl Imidazole	0.35	0.25-0.75		
	Filler	Dolomite	10.6	0-45		
	Wax	Polypropylene	1.8	1.0-4.5		
60				•	•	60
	Example 2					
	A white pigme	ented coating as in Exam	mple 1A wa	s sprayed onto 6' 6	6" × 2'6" hardboard flush	
	doors. The power	der was applied using 3	electrostati	c Powder spray gu	ns mounted vertically over	
٥-	tne doors which	were supported on a c	ross rod cor	veyor. The powder	was applied uniformly to	
66	a film weight of	50 gms/sq metre (40	microns thic	ckness) after an init	ial dusting process. The	65

5	coated door was conveyed under Infra Red lamps of 1 micron wavelength for a total time of 75 seconds, during which the powder fused and cured. Following a short air jet cooling section, the doors were off loaded and stacked. The resultant finish was smooth and very hard, and could be sawn and drilled without damage or loss of adhesion.	5
	Example 3	
10	A beige textured finish powder as in Example 1D was coated onto sheets of fine surface chipboard. The board was supported on a cross rod conveyor, and first passed through a dust removal process. The powder was applied via a vibrated trough, dropping powder vertically onto the board, to give a film weight of 70 gms/sq metre (55 microns film thickness). The powder was fused and cured by passing the board under Infra Red lamps of 2–3 micron wavelength for a total time of 60 seconds. After air jet cooling the boards were off loaded and stacked. The finish had an even, smooth texture, suitable for use in kitchen furniture or shelving.	10
	Various modifications and developments falling within the scope of the present invention will	
15	be apparent to those skilled in the art.	15
13	be apparent to those skilled in the art.	
20	CLAIMS  1. A method of coating a cellulose fibre substrate including the steps of depositing a resincontaining coating powder onto the substrate to form a coating thereon and subsequently using radiant heat to cure the coating on the substrate.  2. A method as claimed in claim 1, wherein the substrate is electrically connected to earth during deposition of the coating powder, the powder being electrostatically charged and caused to impinge on the substrate.	20
	3. A method as claimed in claim 2, wherein the powder is projected towards the substrate	
25	by means of an electrostatically charging spray gun.	25
	4. A method as claimed in claim 2, wherein the powder is arranged to fall on the substrate	
	from a vibratory hopper which is maintained at a suitable electrical potential.	
	5. A method as claimed in any one of claims 2 to 4, wherein the substrate is thin and is	
	backed by an earthed electrically conducting support during deposition of the coating powder	30
30	thereon.	30
	6. A method as claimed in any one of claims 2 to 4, including making a plurality of earth	
	connections to the substrate prior to depositing the coating powder thereon.  7. A method as claimed in claim 1, wherein the powder is arranged to fall on to the	
	substrate from an earthed vibtratory hopper so that the powder is uncharged.	
35		35
33	radiation.	
	9. A method as claimed in claim 8, wherein the infra-red radiation has a wavelength in the	
	range 1.0 to 5 microns.	
	10. A method as claimed in claim 8, wherein the wavelength of the radiation lies in the	40
40	range 1.0 to 1.5 microns.	40
	11. A method as claimed in claim 9, wherein the intensity of the radiation incident on the	
	powder is between 1 to 10 watts per centimetre of length of the radiation source.  12. A method as claimed in any one of claims 8 to 11, wherein the infra-red radiation is	
	provided by lamps spaced between 2 and 20 cms from the powder coating.	
45	13. A method as claimed in any one of claims 1 to 12, wherein the resin has a softening	45
70	temperature between 70°C and 120°C.	
	14. A method as claimed in any one of claims 1 to 13, wherein the resin has a Tg of	
	between 40°C and 80°C.	
	15. A method as claimed in any one of claims 1 to 14, wherein the resin has a melt index	EΛ
50	between 2 gm/min and 30 gm/min (ASTM D1238-62T).	50
	16. A method as claimed in any one of claims 1 to 15, wherein the resin has a density of	
•	from 1.1 to 1.4 gm/ml.	
	17. A method as claimed in claim 16, wherein the resin is a polyester and the curing agent is triglycidyl isocyanurate or tri(epoxypropyl) isocyanurate.	
55	and the second s	55
55	and the curing agent is an isocyanate or an epoxy resin.	
	19. A method as claimed in any one of claims 1 to 16, wherein the resin is an epoxy resin	
	and the curing agent is substituted dicyandiamide, an amine, an amidine or an anhydride.	
	20. A method as claimed in any one of claims 1 to 16, wherein the resin is an acrylic, an	
60	epoxy-phenolic, an epoxy-novolac or an epoxy-resol.	60
	21. A method as claimed in any one of claims 1 to 20, wherein the coating powder	
	comprises a flow agent.	
	22. A method as claimed in claim 21 wherein the flow agent is a polyacrylate, fluorocarbon,	
65	a silicone polymer or a polyvinyl butyral polymer.  23. A method as claimed in claim 21 or claim 22, wherein the flow agent is present in an	65
65	23. A method as claimed in claim 21 or claim 22, wherein the flow agent is present in an	- •

	amount of at least 0.1 parts by weight based on 100 parts of the resin.	
	24. A method as claimed in claim 23, wherein the flow agent is present in an amount in the range of from 0.2 to 10 parts.	
	25. A method as claimed in claim 24, wherein the flow agent is present in an amount in the	
5	range of from 0.4 to 5 parts.	5
	26. A method as claimed in any one of claims 1 to 25, wherein the coating powder	
	comprises an adjuvant for lowering the softening temperature of the resinous composition.	
	27. A method as claimed in claim 26, wherein the adjuvant is a wax.	
10	28. A method as claimed in claim 27, wherein the wax is a polyolefin wax. 29. A method as claimed in claim 27, wherein the wax is an amide wax.	10
	30. A method as claimed in claim 27, wherein the wax is a crystalline or microcrystalline	. •
	wax,	
	31. A method as claimed in any one of claims 27 to 30, wherein the wax is present in an	
	amount of up to 10 parts by weight based on 100 parts of the resin.	
15	32. A method as claimed in any one of claims 27 to 31, wherein the wax is present in an	15
	amount of at least 0.1 parts by weight based on 100 parts of the resin.	
	33. A method as claimed in claim 32, wherein the wax is present in an amount of from 0.5 to 10 parts by weight based on 100 parts of the resin.	
	34. A method as claimed in claim 33, wherein the wax is present in an amount of from 1 to	
20	5 parts by weight based on 100 parts of the resin.	20
	35. A method as claimed in claim 26, wherein the adjuvant is a plasticiser.	
	36. A method as claimed in any one of claims 1 to 35, wherein the coating powder	
	comprises a pigment.	
0.5	37. A method as claimed in claim 36, wherein the pigment is titanium dioxide.	25
25	38. A method as claimed in claim 36, wherein the pigment is carbon black.  39. A method as claimed in any one of claims 36 to 38, wherein the pigment is present in	25
	an amount of from 0.5 to 200 parts by weight based on 100 parts of the resin.	
	40. A method as claimed in claim 39, wherein the pigment is present in an amount of from	
	10 to 50 parts by weight based on 100 parts of the resin.	
30	41. A method as claimed in any one of claims 1 to 40, wherein the coating powder	30
	comprises an extender.	
	42. A method as claimed in claim 41, wherein the extender is calcium carbonate or barium	
	sulphate.	
32	43. A method as claimed in any one of claims 41 or 42, wherein the extender is present in an amount of from 5 to 50 parts by weight, based on 100 parts of the resin.	35
33	44. A method as claimed in any one of claims 1 to 43, wherein the coating powder	-
	comprises an ultra-violet absorbent, an accelerator, an anti-cratering agent, a fungicide or a	
	mixture of any two or more of said adjuvants.	
	45. A method as claimed in claim 1, wherein the coating powder is as described in Example	
40	1 herein.	40
	46. A method as claimed in claim 1, carried out substantially as described in either of	
	Examples 2 or 3 herein.  47. A method of coating a wood-based board substrate, wherein a coating powder	
	comprising 100 parts by weight of a thermosetting resin, a curing agent for the resin, at least	
45	0.1 parts by weight of a flow agent and up to 10 parts by weight of a wax is electrostatically	45
	deposited on the surface of the substrate and is then cured by infrared irradiation.	
	48. A cellulose fibre substrate which has been coated by a method as claimed in any one of	
	claims 1 to 42.	
EO	49. A cellulose fibre substrate as claimed in claim 48, which is timber.	50
50	<ol> <li>A cellulose fibre substrate as claimed in claim 48, which is a compressed board.</li> <li>A cellulose fibre substrate as claimed in claim 48, which is paper.</li> </ol>	50
	OT. A Condition intro substrate as claimed in Claim 40, which is paper.	